

PATHWAYS TO REDUCTION OF CO₂ EMISSIONS FROM COMBUSTION ENGINES

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OUTLINE

- Part 1: Technology Screening to meet 2025 CO₂ Emissions Regulations (Co-PI) – On-going
- Part 2: Fundamental Exhaust Gas Recirculation (EGR) Cooler Fouling and Mitigation Study (PI) - Completed
- Quick overview of other projects

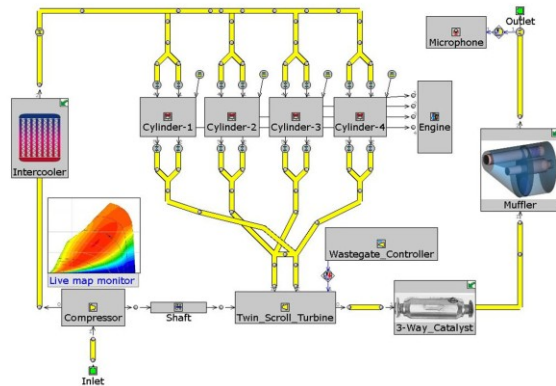
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OBJECTIVE

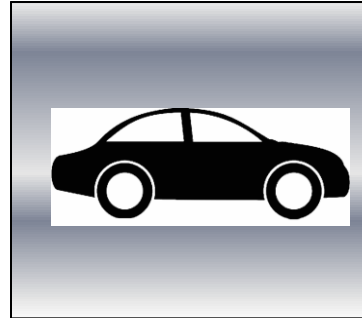
- *Explore diesel engine technology combinations that meet 2025 CO₂ regulations consistent with future emissions standards*
- *Remain cost competitive*

METHODOLOGY



1-D Engine Model

+



Vehicle Model

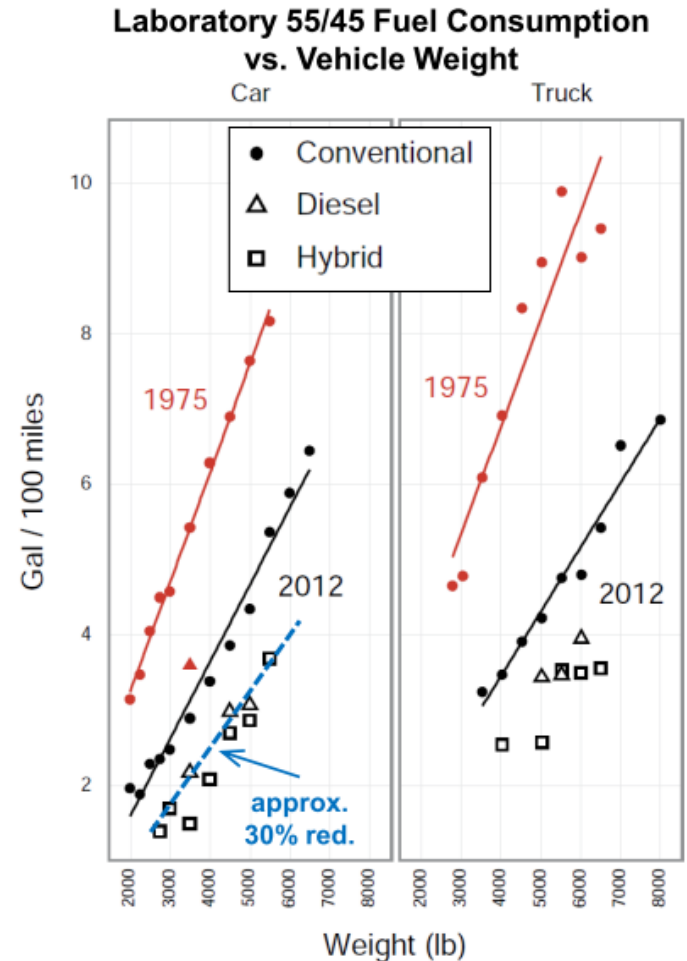


$\text{CO}_2 \text{ (g/km)}$

- CO_2 emissions estimated for different diesel engine technologies over the New European Driving Cycle (NEDC) and the Worldwide Harmonized Light Vehicles Test Procedure (WLTP)

DIESEL ADVANTAGE OVER GASOLINE

- Data from EPA show approximately 30% reduction in gallons/100 miles for diesel (approx. 40% higher MPG)
- Why is a diesel engine more efficient than a conventional gasoline engine?
Common answers:
 - No throttling losses
 - Higher compression ratio
- These are contributors, but the lean combustion process of the diesel engine is the main factor leading to efficiency gain

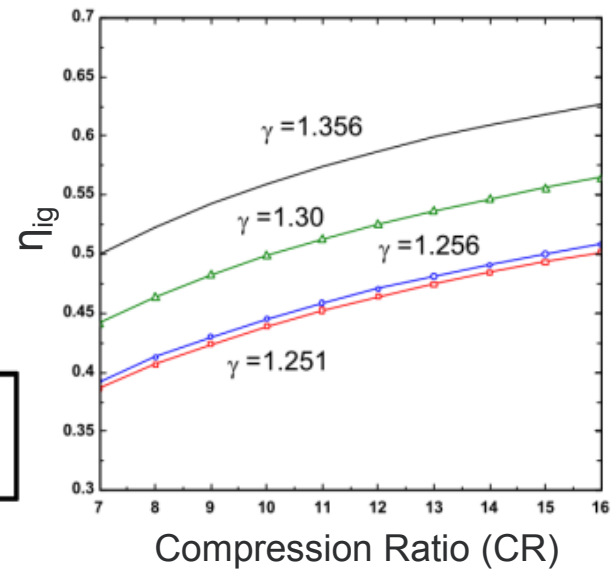
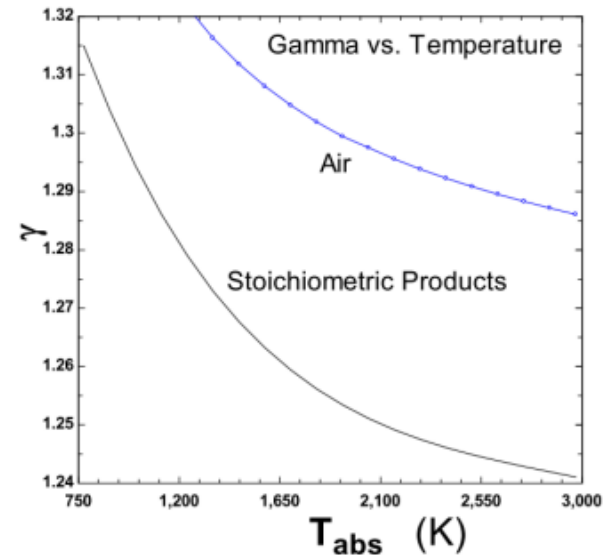


Source: Light-Duty Automotive Technology, Carbon Dioxide Emissions, and Fuel Economy Trends: 1975 Through 2012, EPA, 2013

LEAN COMBUSTION

- Increased dilution improves indicated fuel conversion efficiency by lowering temperatures and increasing gamma (ratio of specific heats).
- Switching from exhaust dilution to air dilution improves indicated fuel conversion efficiency by increasing gamma.
- Increased dilution improves the indicated efficiency by lowering temperatures and decreasing heat losses.

$$\eta_{ig} = 1 - \frac{1}{CR^{\gamma-1}}$$

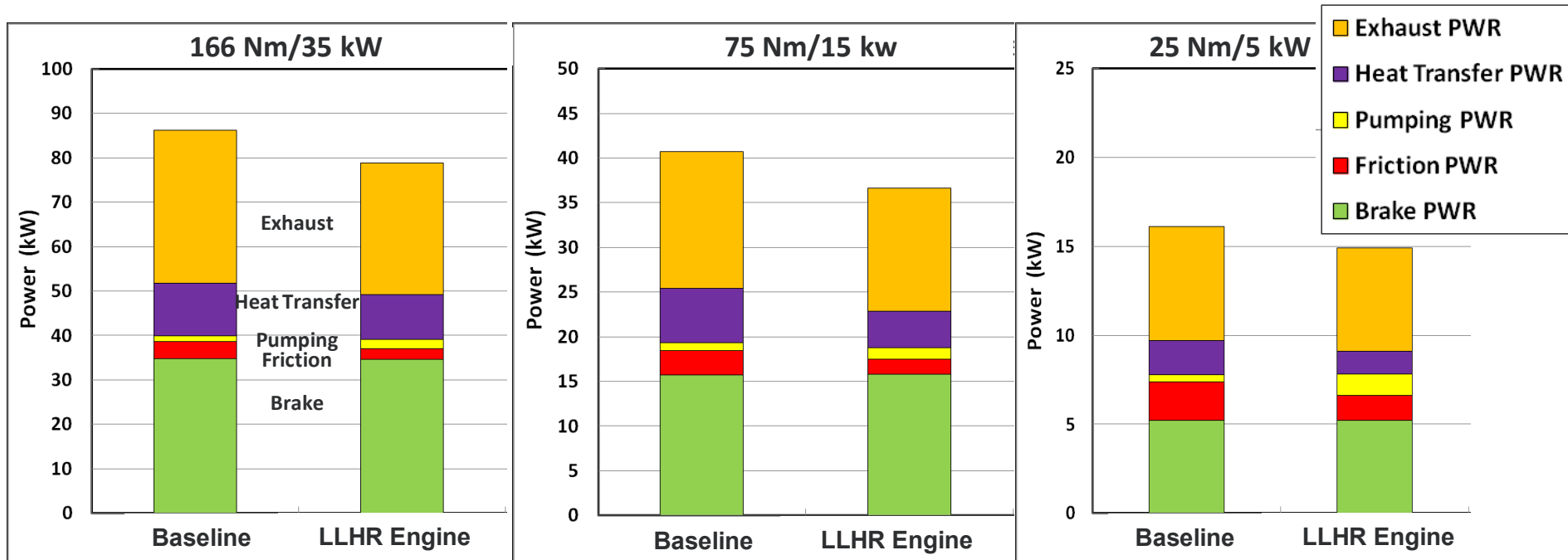


Source: Foster, Combustion Engines Efficiency Colloquium, DOE 2010

LOW HEAT REJECTION

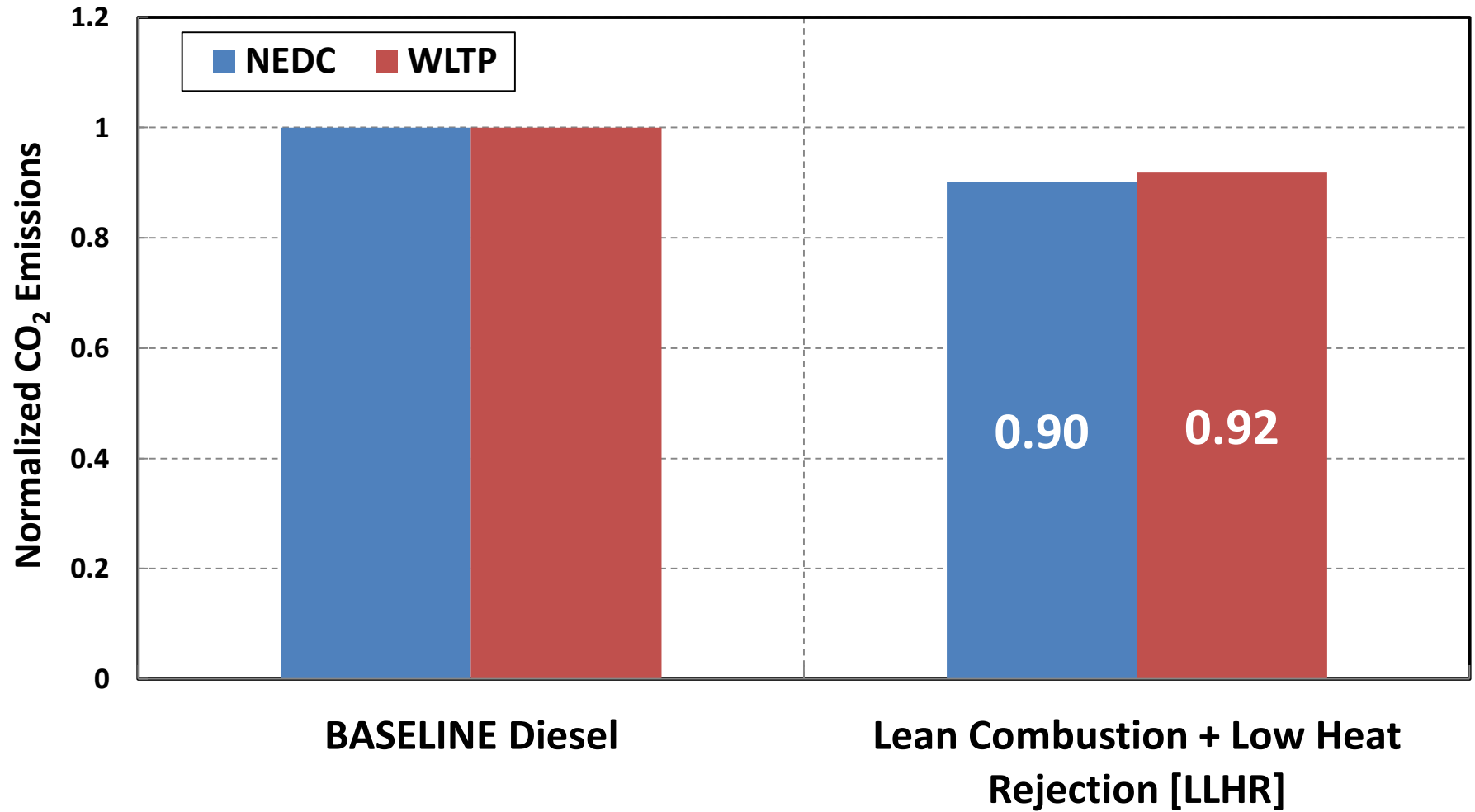
- In-cylinder heat losses in modern diesel engines constitute a significant part of thermodynamics losses.
- Engine efficiency can be increased by retaining a greater amount of combustion energy for conversion to mechanical work.
- Sensitivity studies show that, provided heat losses could be minimized, there is potential for significant fuel consumption improvement.
- Several pathways to achieve low heat rejection.

BASELINE DIESEL vs LEAN LOW HEAT REJECTION (LLHR) ENGINE FUEL ENERGY BREAKDOWN



- Combined pumping and friction torques are comparable
 - Boosting system for lean combustion adds more pumping torque
- Due to leaner combustion and higher *effective* expansion ratio the LLHR engine is more efficient
 - Centroid of heat release closer to TDC for similar peak cylinder pressure and cylinder temperatures
- Lower energy in the exhaust

CO₂ EMISSIONS



SUMMARY

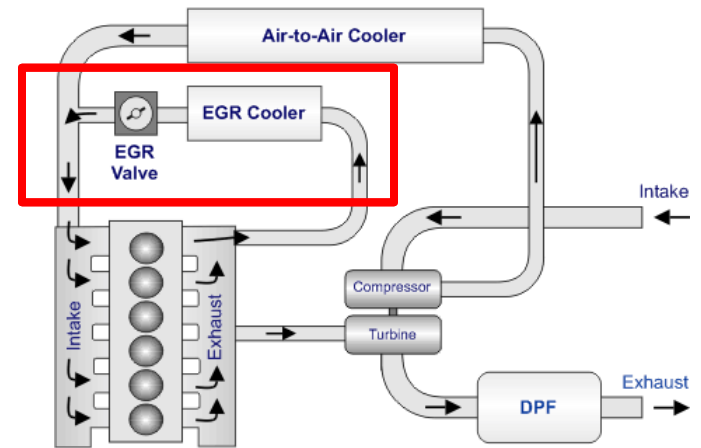
- Developing robust, cost-effective, lean combustion and low heat rejection diesel engines will be challenging but the fuel economy benefits are significant.
- Challenges for engine optimization:
 - Robust combustion control over all operating conditions
 - Robust emissions control over all operating conditions
 - Good fuel consumption under real world driving conditions
 - Low combustion noise
 - Exhaust temperature
- This will require a coordinated effort between air handling, combustion, aftertreatment and controls – a system optimization approach.
- In order for this to work effectively it is important to focus research on fundamental insights that have long-term value critical to achieving upper-bound efficiency and lower-bound emissions.

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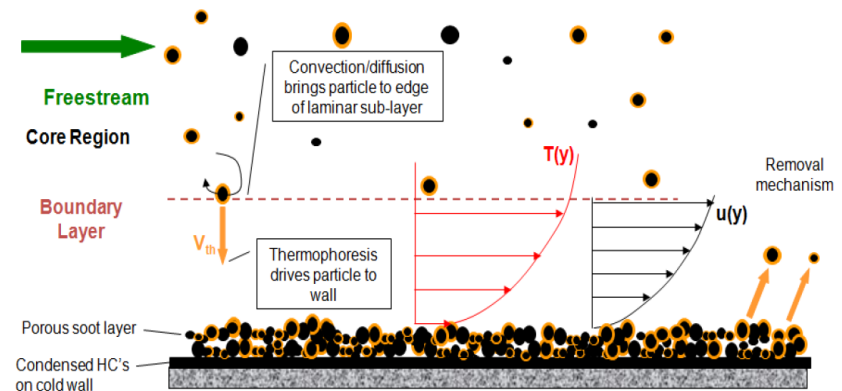
EXHAUST GAS RECIRCULATION (EGR) COOLERS

- EGR coolers are compact heat exchangers used on all modern diesel engines to cool exhaust gasses that are re-circulated into the combustion chamber.
- Exhaust gas recirculation is used to control NO_x (oxides of nitrogen) emissions that result from diesel combustion.
- Advanced diesel combustion strategies to improve fuel economy rely on cooled exhaust gas recirculation (EGR).



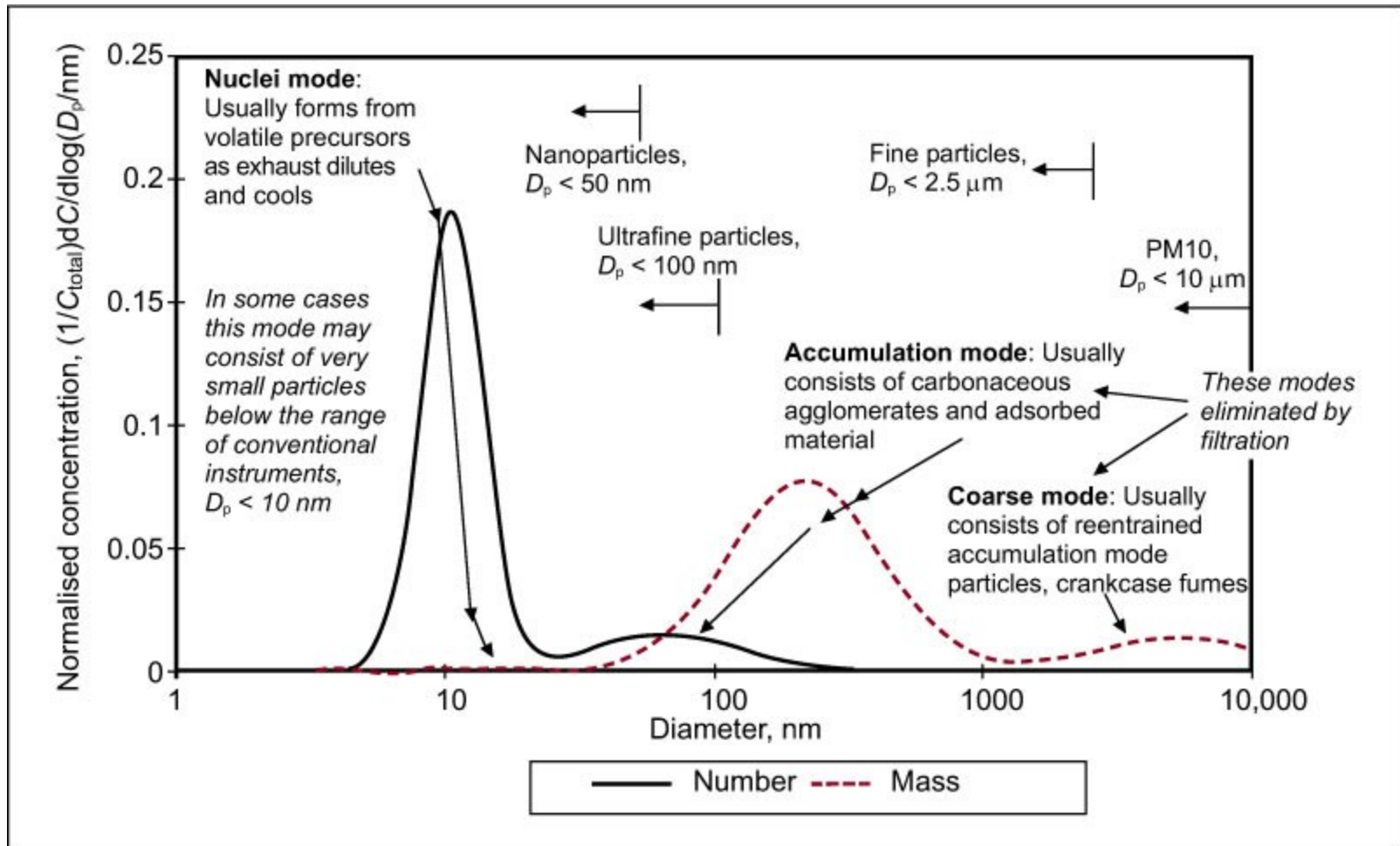
EGR COOLER FOULING

- Fouling of exhaust gas re-circulation (EGR) coolers can result in significant deterioration of the cooler effectiveness and increased pressure drop across the cooler.
- EGR cooler fouling can adversely affect the combustion process, engine durability and emissions.
- Complicated flow physics with multiple soot particle deposition and removal mechanisms. Hydrocarbon and water condensation in addition to soot deposition.
- Goal of this research was to develop a fundamental understanding of EGR cooler fouling mechanisms and demonstrate novel concepts to mitigate fouling and regenerate fouled EGR coolers.



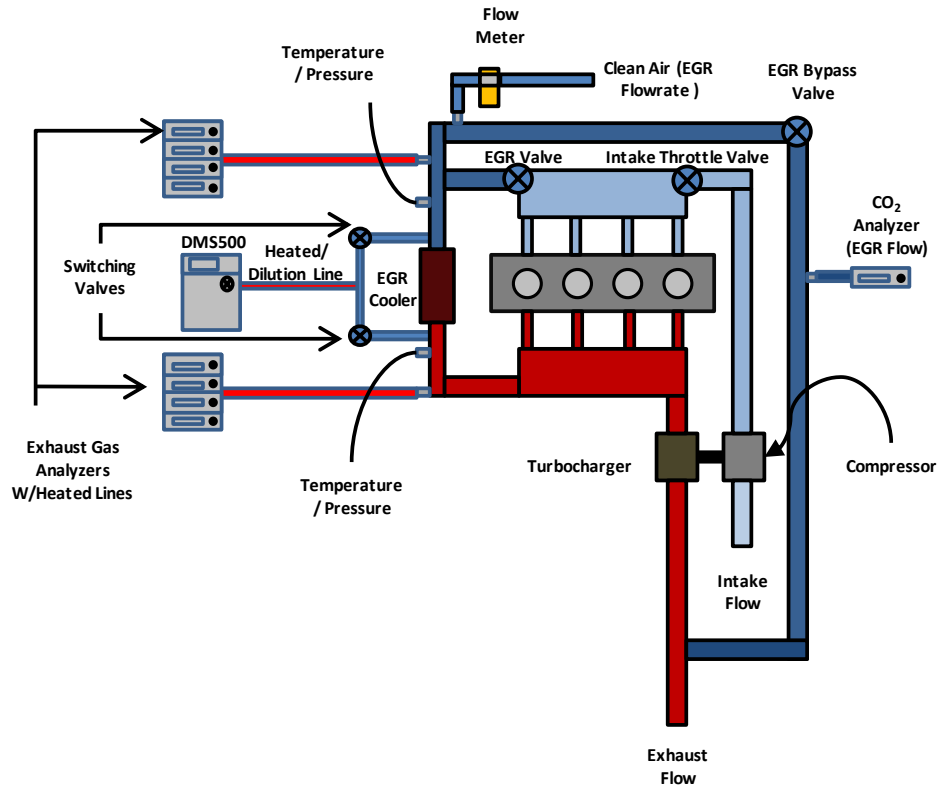
Source: SAE 2010-01-1211

DIESEL EXHAUST PARTICLE EMISSIONS

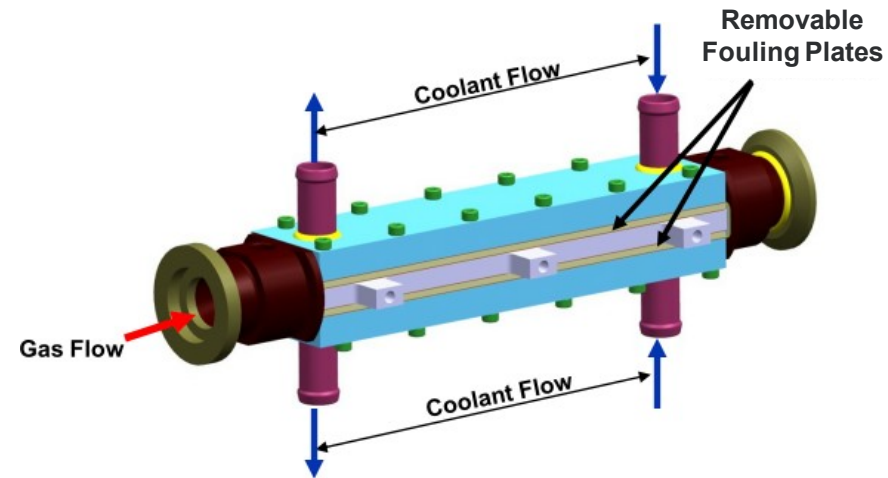


Source: David Kittelson, University of Minnesota

EXPERIMENTAL SETUP

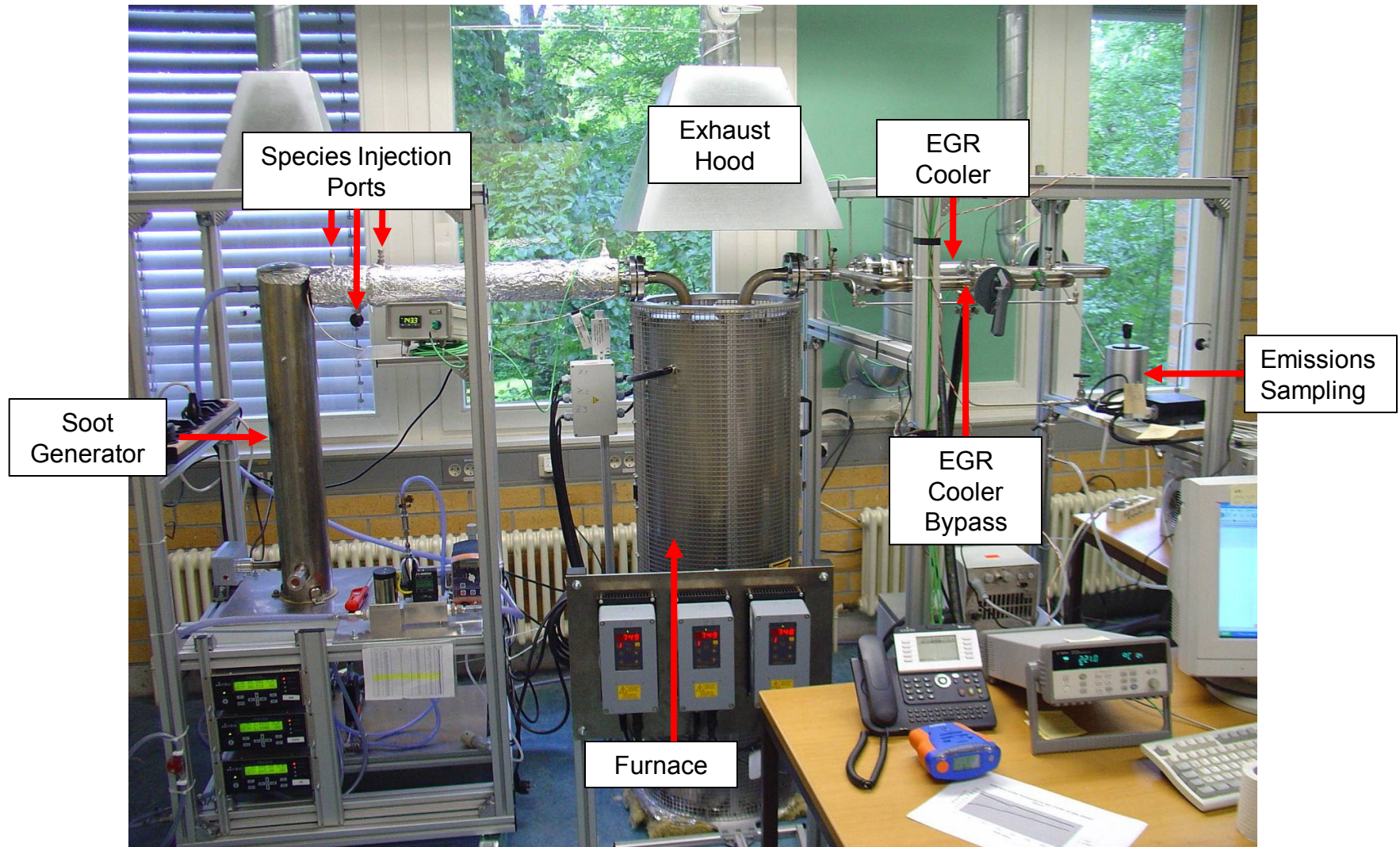


**Engine Test Stand
at GM R&D**



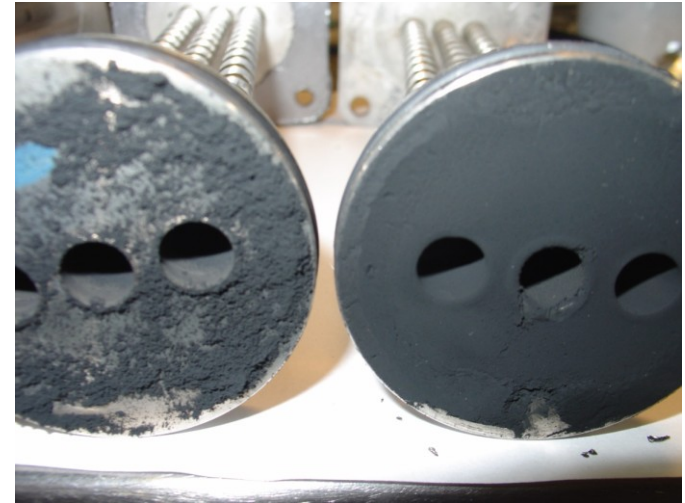
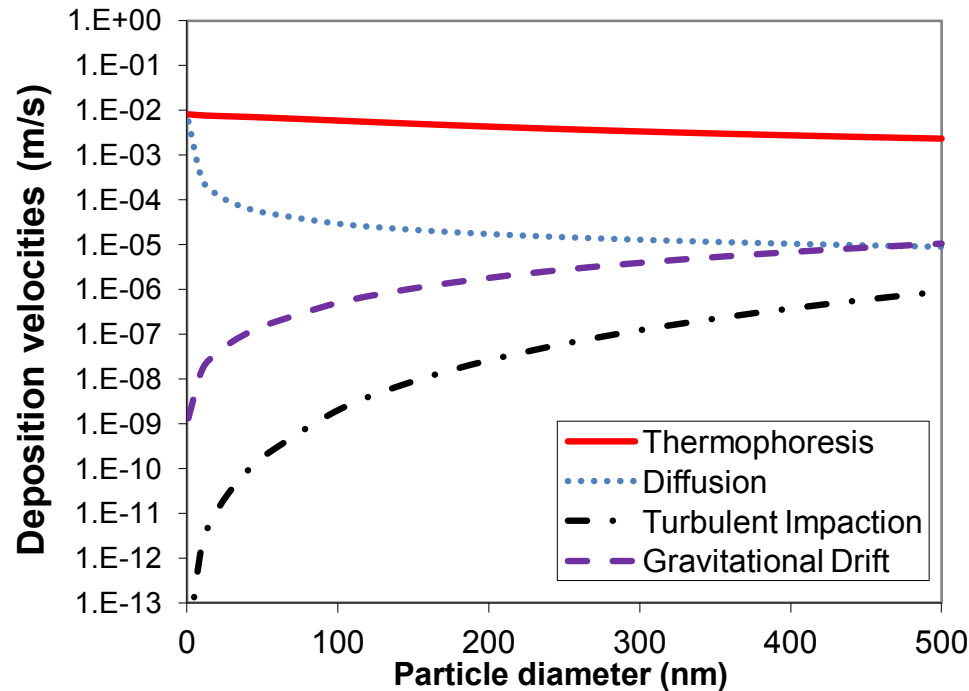
**Single Rectangular Channel
EGR Cooler**

EXPERIMENTAL SETUP



Lab Reactor – University of Stuttgart

THERMOPHORESIS



Left: $\Delta T \sim 0^\circ\text{C}$
(Isothermal)

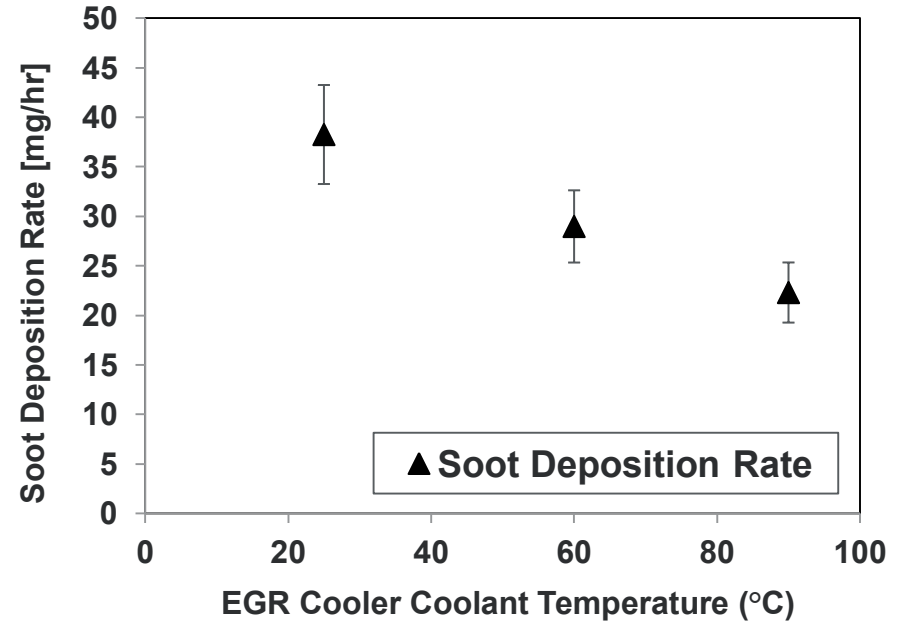
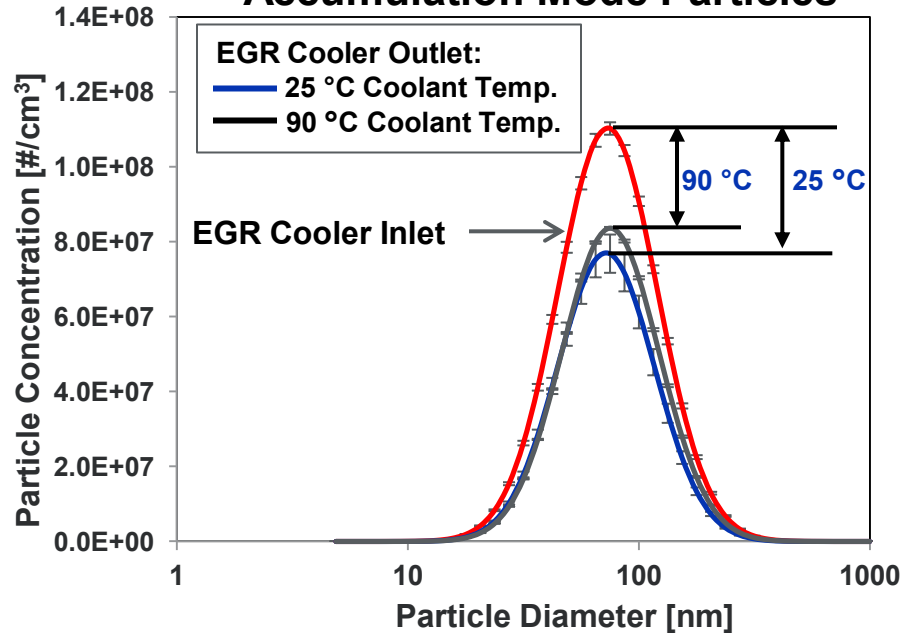
Right: $\Delta T \sim 300^\circ\text{C}$
(Thermophoresis)

- Thermophoresis* is the dominant mechanism for particle deposition in EGR coolers.
- Fouling will always occur as a result of the temperature difference, which is necessary for heat exchanger operation.

* Thermophoresis = Particle transport due to temperature difference (ΔT)

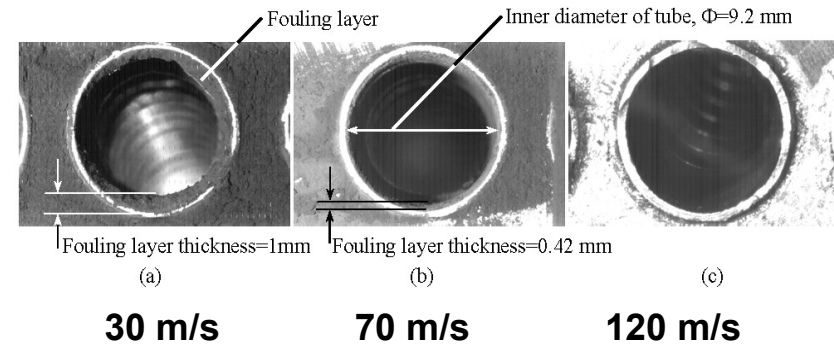
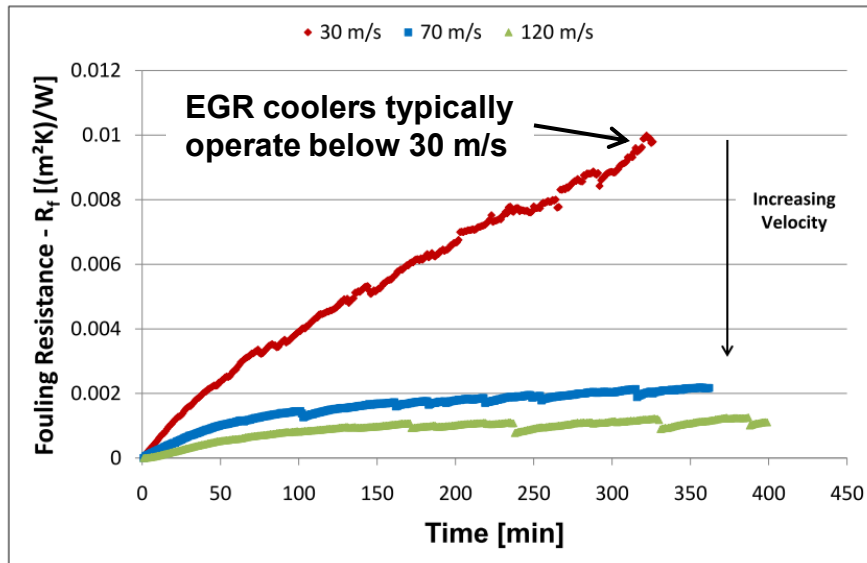
THERMOPHORESIS

Accumulation Mode Particles



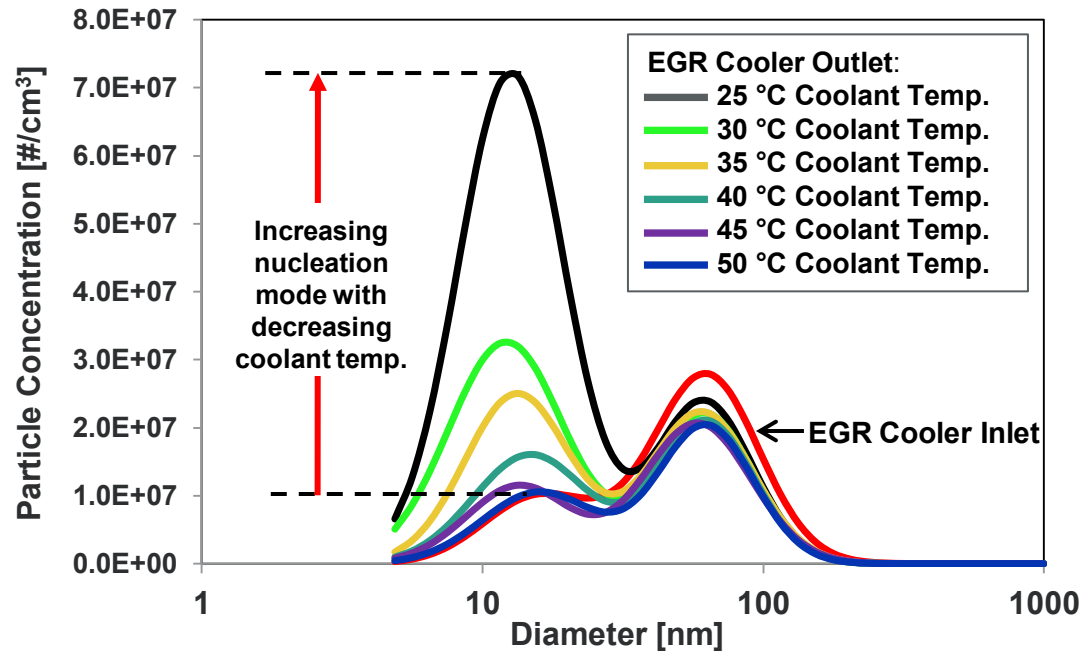
- Particle measurements upstream and downstream of the EGR cooler also show evidence of thermophoresis.
- Soot deposition rate due to thermophoresis increases with decrease in coolant temperature.

PARTICLE REMOVAL



- Increasing wall shear stress due to gas velocity appears to be effective in preventing dry soot accumulation on the cooler walls.
- However, typical gas velocities through the EGR cooler are considerably lower than 30 m/s for reasons of excessive pressure drop.
- It is impractical to generate the high gas velocities necessary for deposit removal through the cooler of a conventional diesel engine.

PARTICLE FORMATION



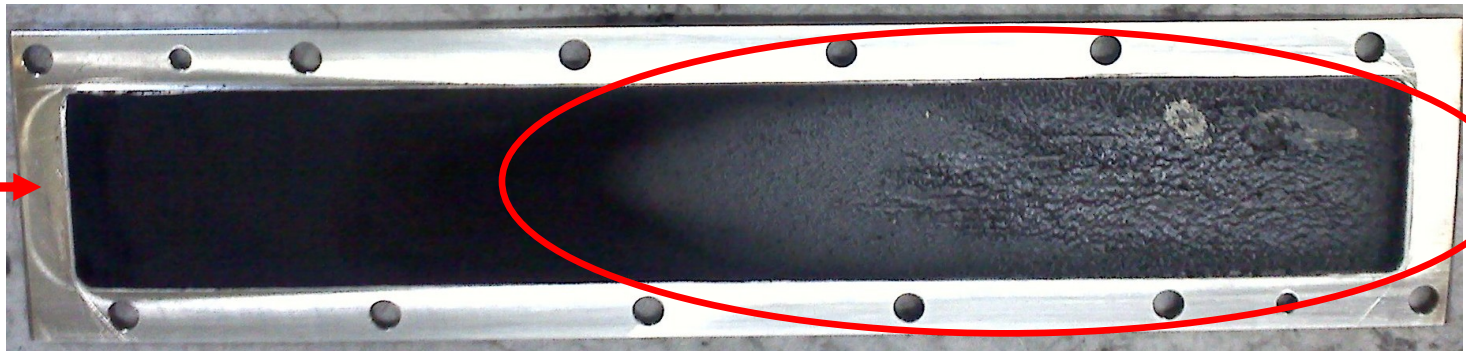
- As the coolant temperature is decreased below 45 °C, nucleation mode particle concentration begins to increase downstream of the cooler. This trend is continued as the coolant temperature is decreased further.
- Condensation of hydrocarbons occurs not only on the cooler walls but also in the bulk gas.

EFFECT OF HYDROCARBON (HC) CONDENSATION

$T_{in} = 215^{\circ} \text{C}$
FSN = 2.0
THC = 40 ppm C3 →
Flow: 200 SLPM
Exposure : 2 hours
Tcoolant: 25 C



$T_{in} = 215^{\circ} \text{C}$
FSN = 2.0
THC = 250 ppm C3 →
Flow: 200 SLPM
Exposure : 2 hours
Tcoolant: 25 C

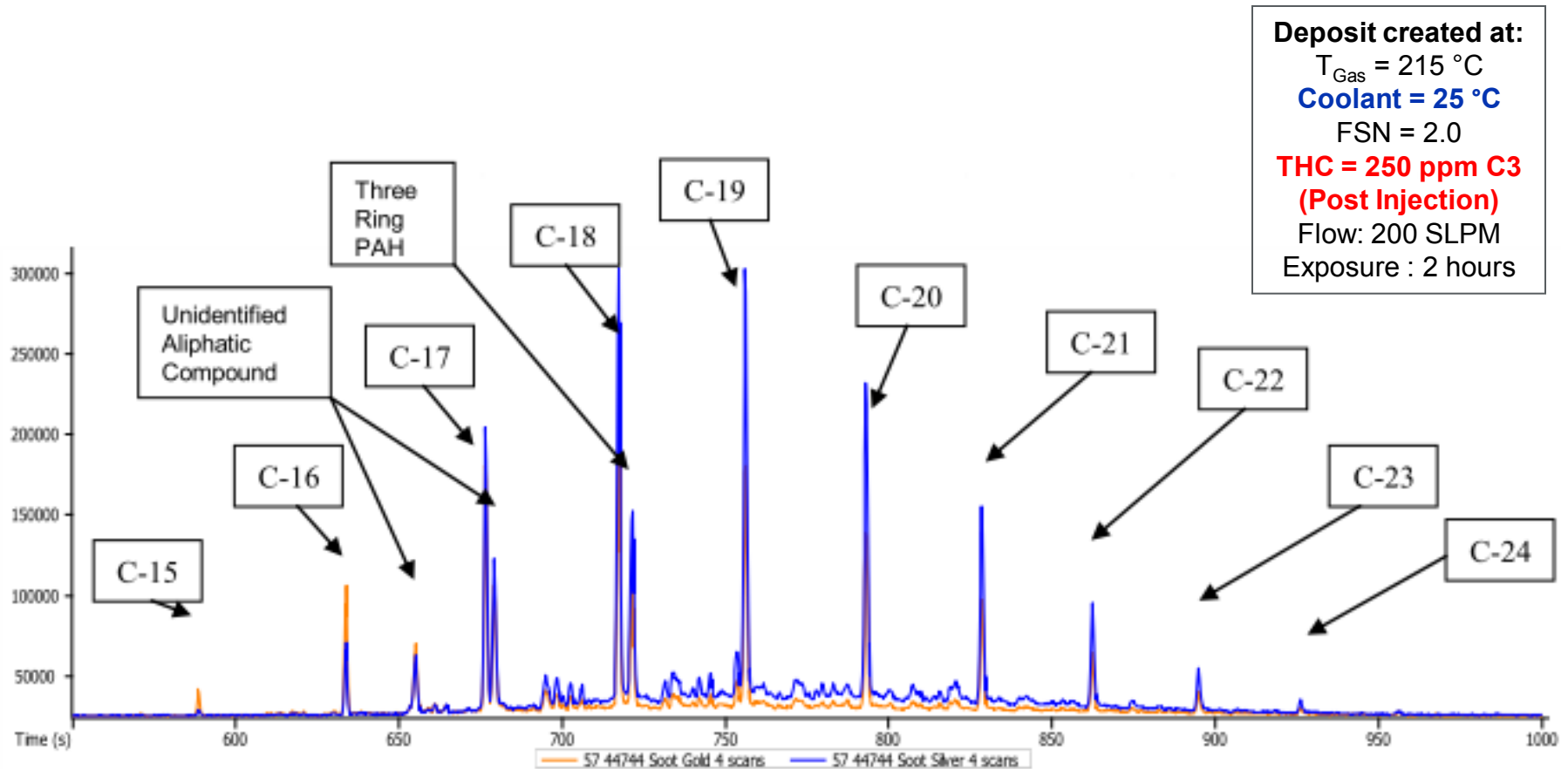


Inlet

Outlet

- Significant changes in deposit morphology were observed due to hydrocarbon condensation.
- Condensed HC's in the EGR cooler diffuse through the deposit layer and stay near the cold wall. Cold wall inhibits evaporation of condensed HC's.

DEPOSIT ANALYSIS



- Heavier hydrocarbons in diesel fuel tend to condense at coolant/wall temperatures typically encountered in EGR coolers.

EFFECT OF WATER VAPOR CONDENSATION

Prior to Water Vapor Condensation

$T_{in} = 215\text{ }^{\circ}\text{C}$

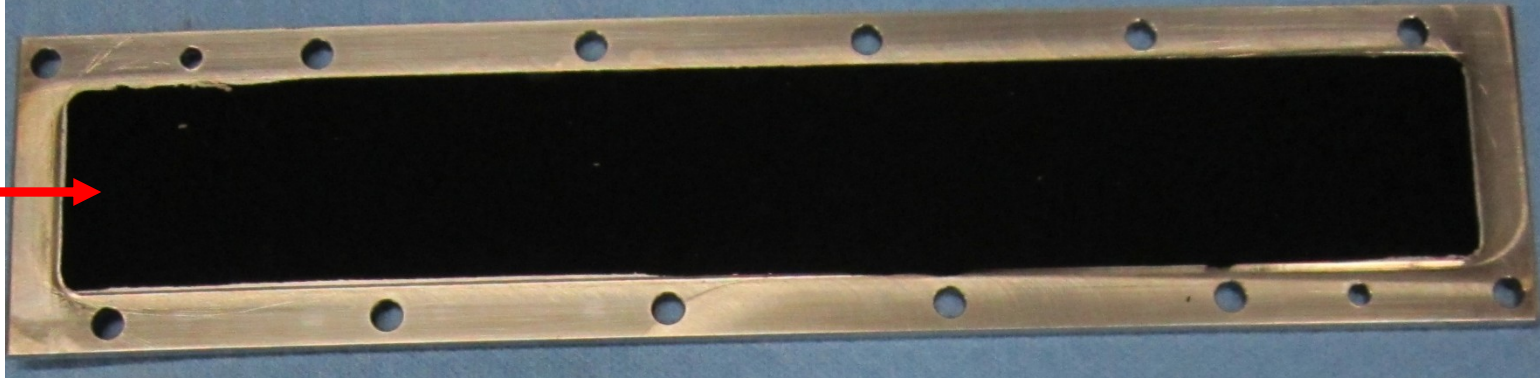
$FSN = 2.0$

THC = 40 ppm C3

Flow = 200 SLPM

Exposure = 2 hours

Coolant = $100\text{ }^{\circ}\text{C}$



After Exposure to Water Vapor Condensation

$T_{in} = 145\text{ }^{\circ}\text{C}$

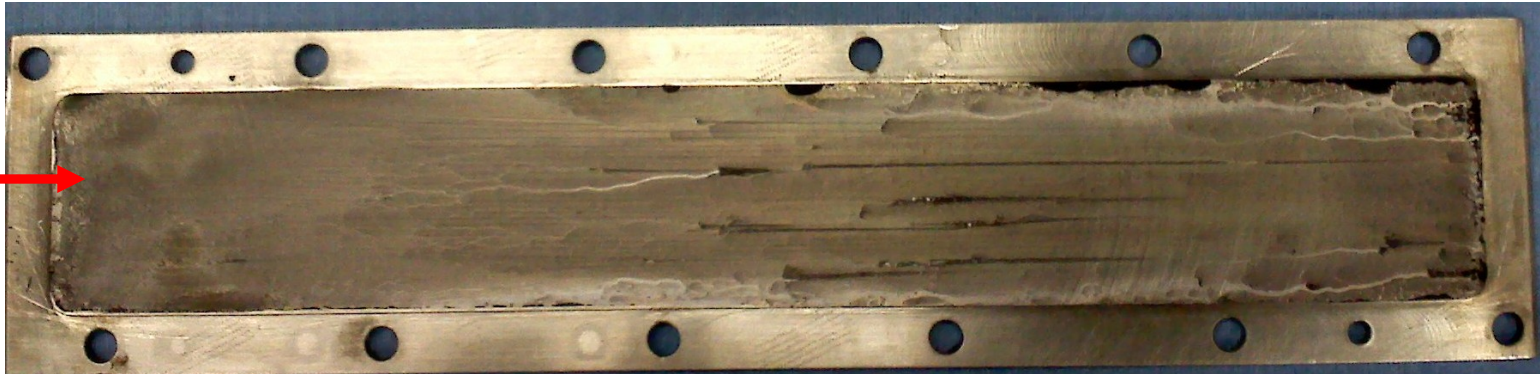
$FSN = 0.3$

THC = 65 ppm C3

Flow = 200 SLPM

Exposure = 30 min

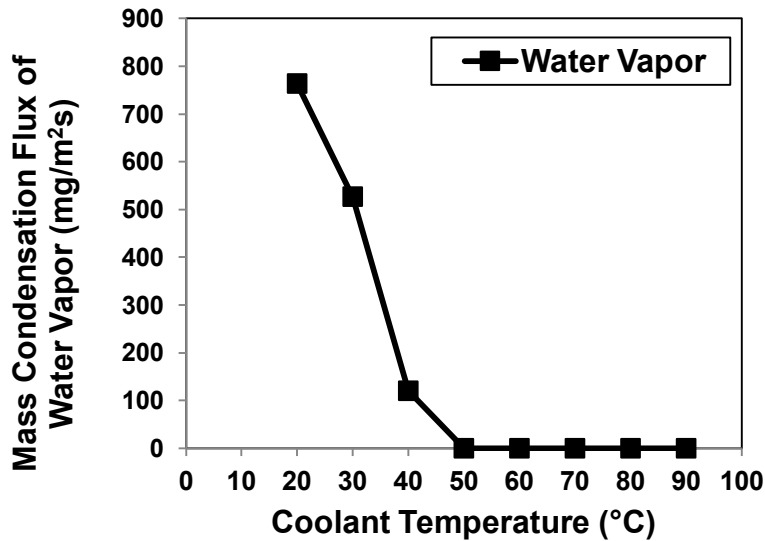
Coolant = $10\text{ }^{\circ}\text{C}$



Inlet

Outlet

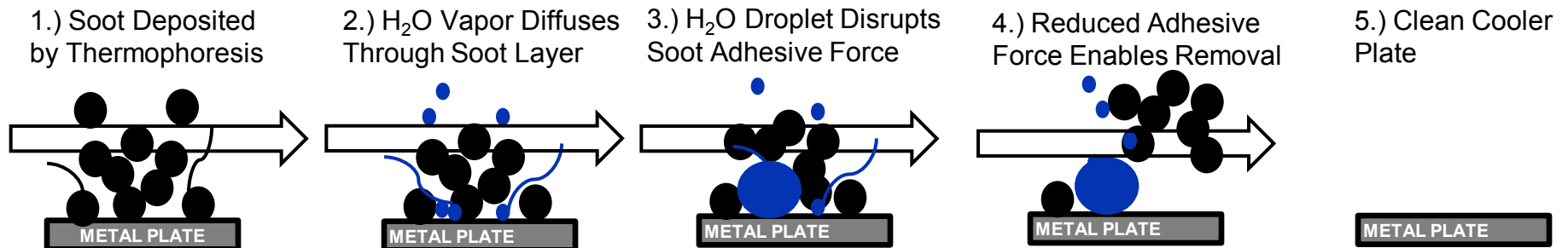
EFFECT OF WATER VAPOR CONDENSATION



Soot Particles/Layer are Hydrophobic

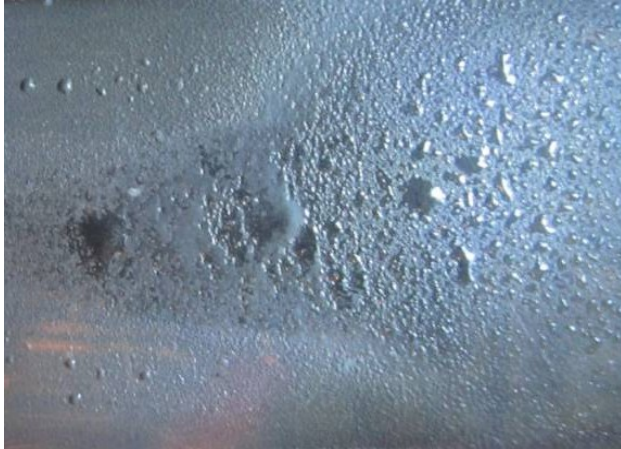


Removal Mechanism

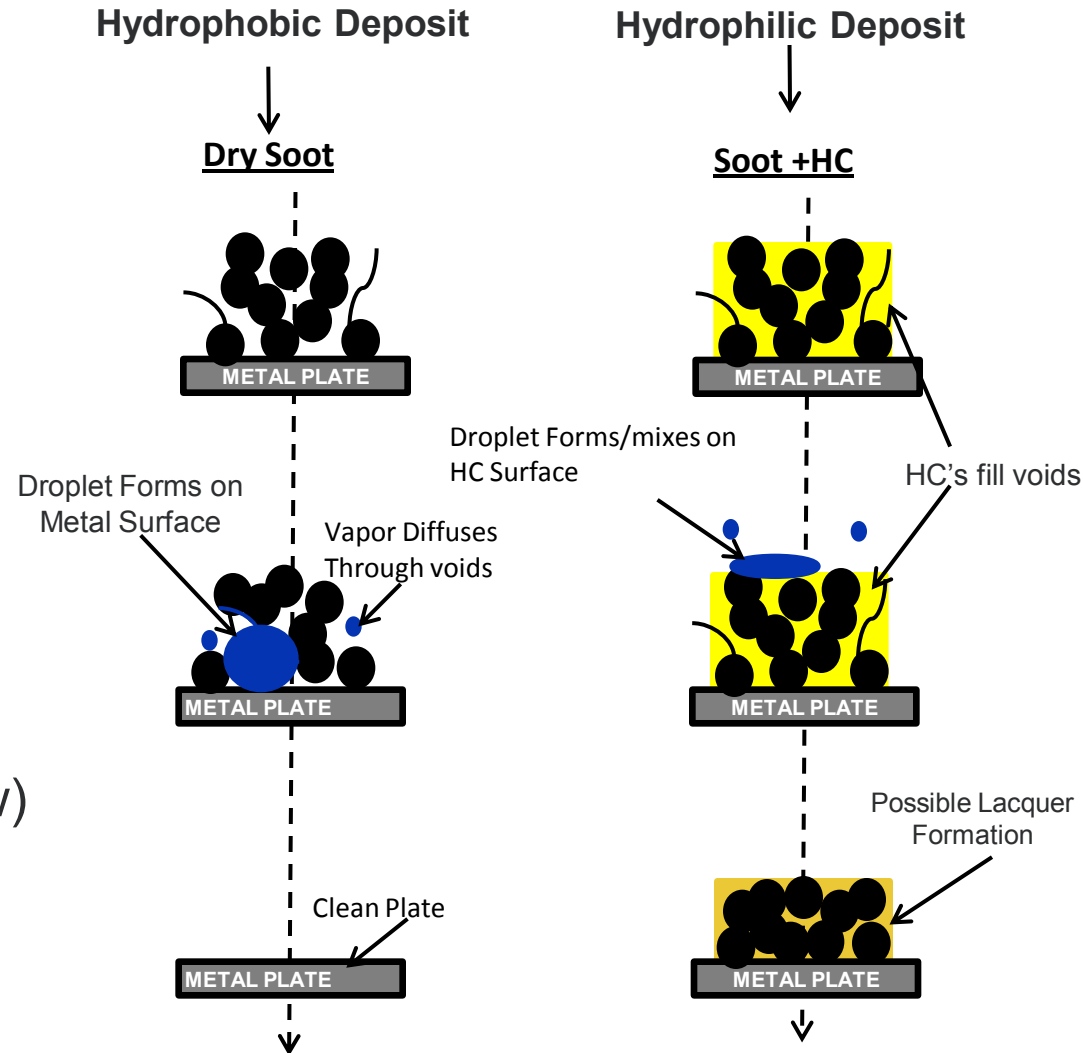


EFFECT OF WATER VAPOR CONDENSATION

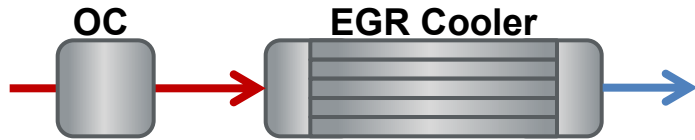
Soot + HC yields Hydrophilic deposit



- Condensation of water vapor occurs on the surface of hydrophilic deposits (not below) and is unlikely to remove deposits.



EFFECT OF OXIDATION CATALYST (OC)

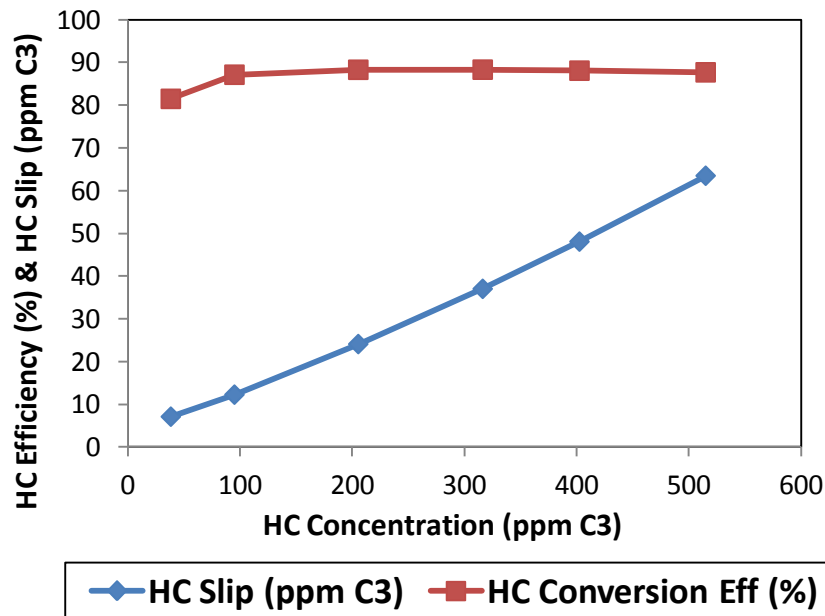


- ➔ Two Catalysts:
 - ➔ Active (Washcoat)
 - ➔ Inactive (NO Washcoat)

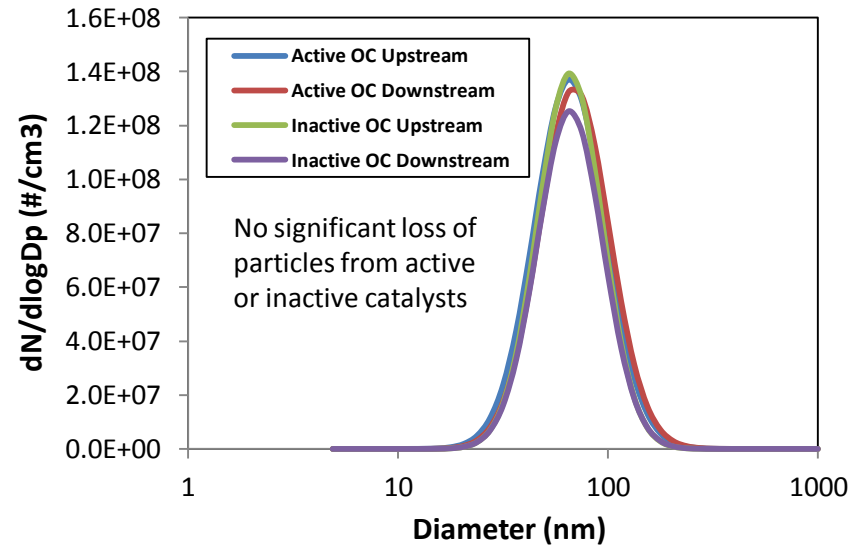
Specifications

Diameter	mm	45
Length	mm	120
Cell Density	cpsi	200 LS
Volume	L	0.19
Washcoat	g/ft ³	67.5 g/ft ³ Pt / 22.5 g/ft ³ Pd

HC Conversion Efficiency

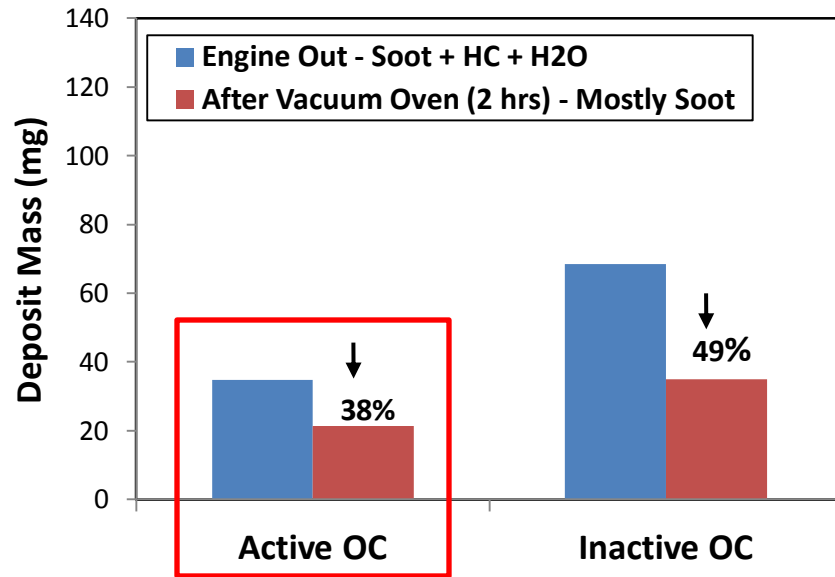


Particle Size Distribution

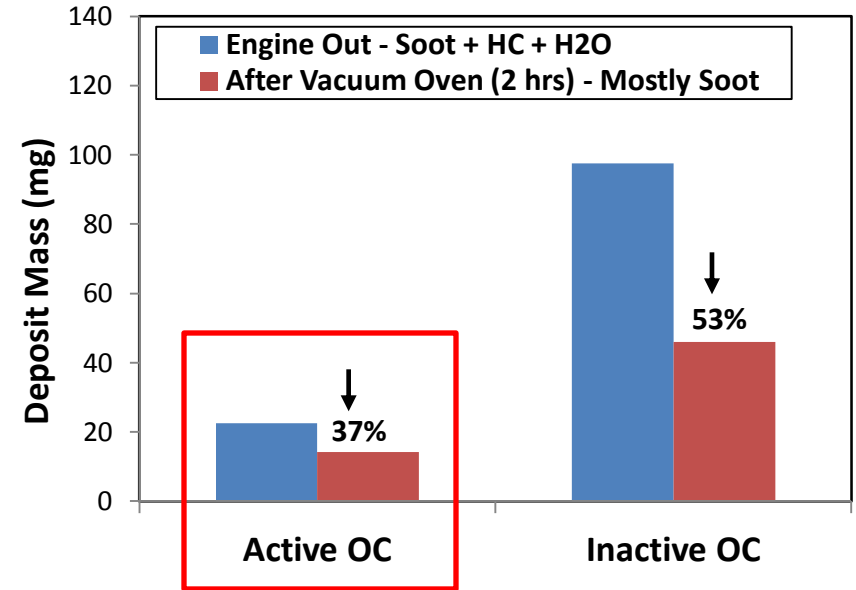


EFFECT OF OXIDATION CATALYST (OC)

50 C Coolant Temperature



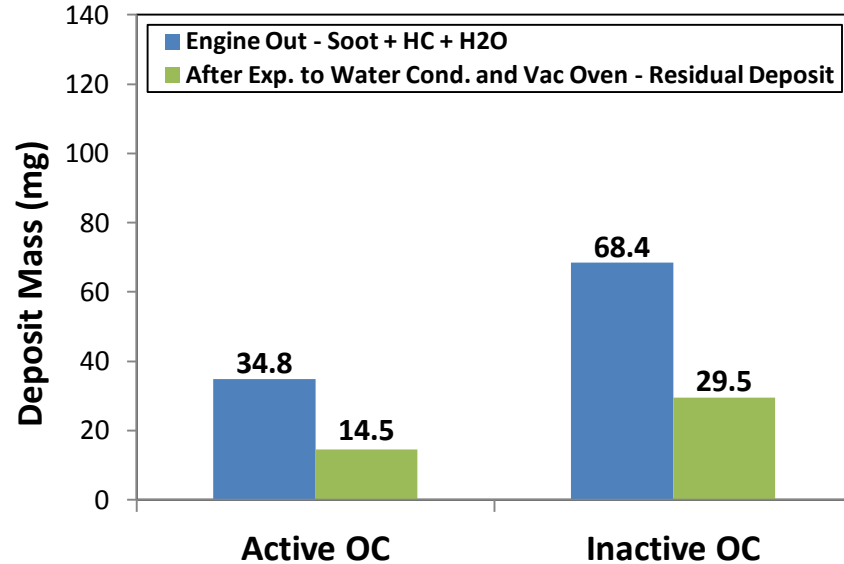
25 C Coolant Temperature



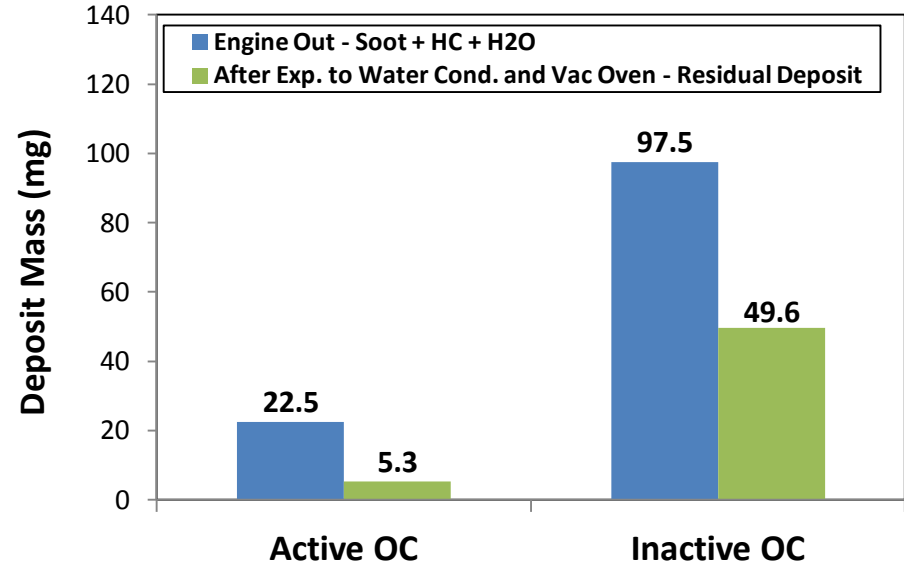
- An oxidation catalyst upstream of the EGR cooler results in lower accumulated deposit mass.

EFFECT OF OXIDATION CATALYST (OC) + WATER VAPOR CONDENSATION

50 C Coolant Temperature



25 C Coolant Temperature



- Exposure to water vapor condensation in addition to the oxidation catalyst results in significant removal of deposit mass.

EFFECT OF OXIDATION CATALYST (OC)

- Saturation Ratio: $SR = \frac{P_v(T)}{P_{sat}(T)}$

$P_v(T)$: Partial pressure of the condensing species

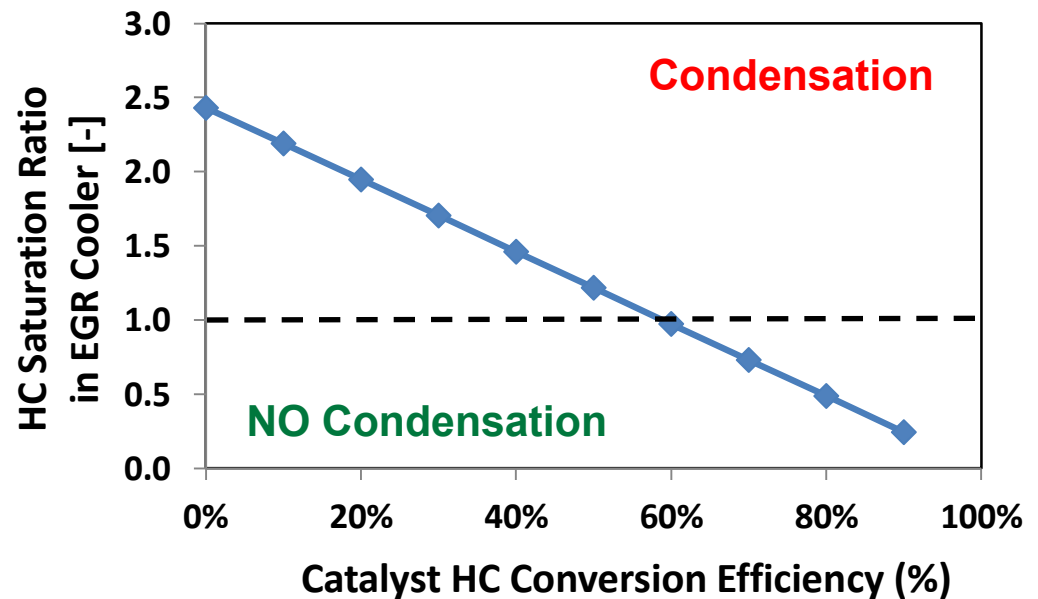
$P_{sat}(T)$: Saturation pressure of the condensing species

- **Condensation typically occurs at $SR > 1.0$**

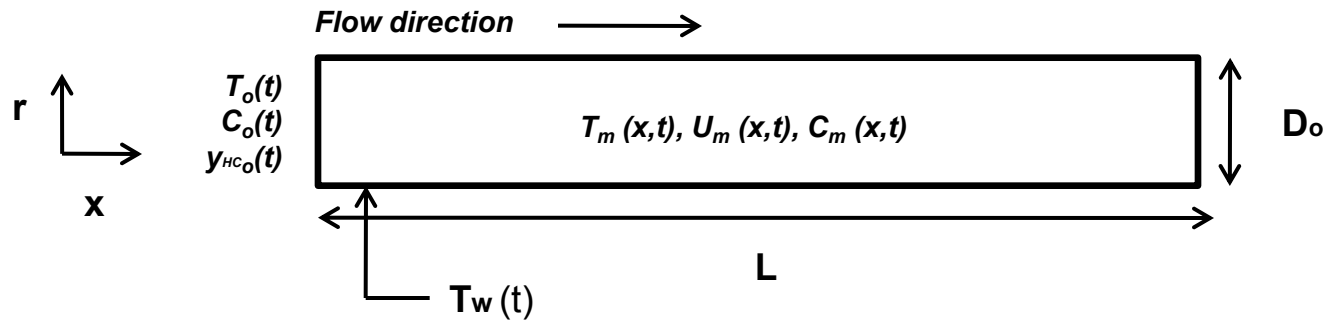
- EGR Coolant Temperature: 50 C

- Engine-out THC: 250 ppm C3

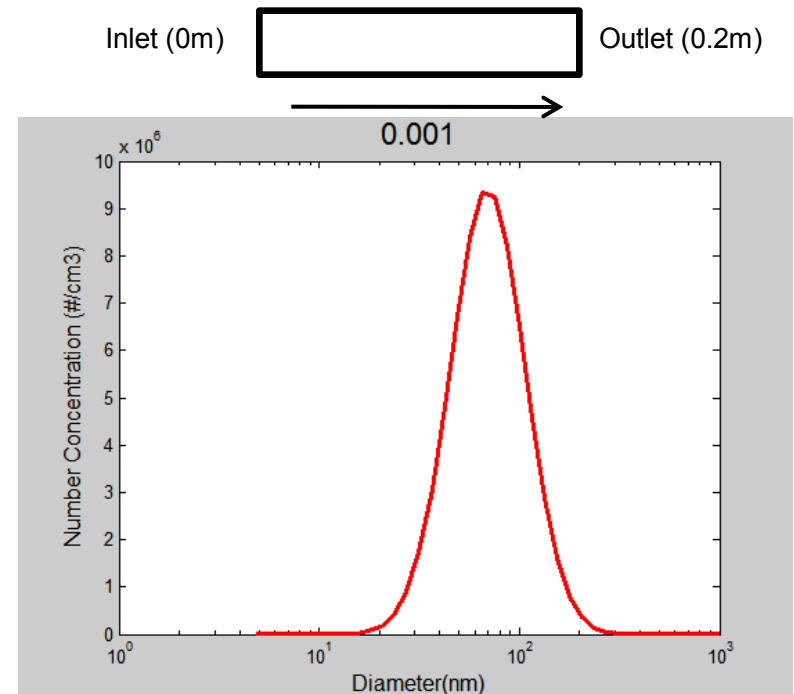
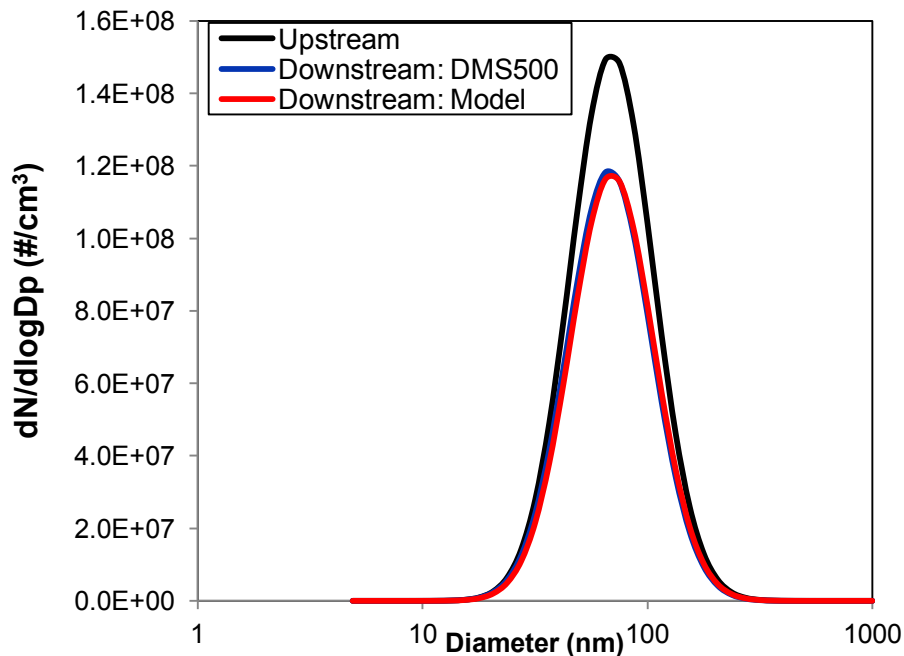
- 100% of the exhaust HC are assumed to be n-hexadecane ($C_{16}H_{34}$)



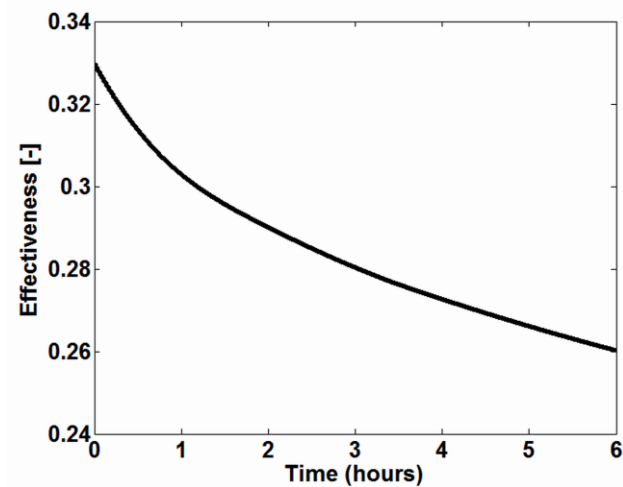
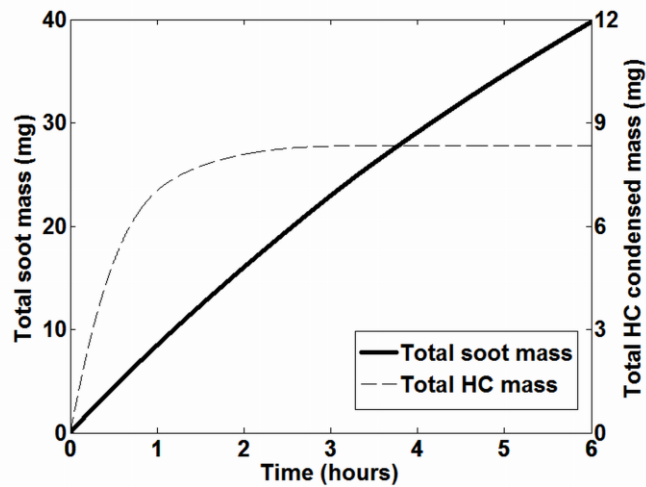
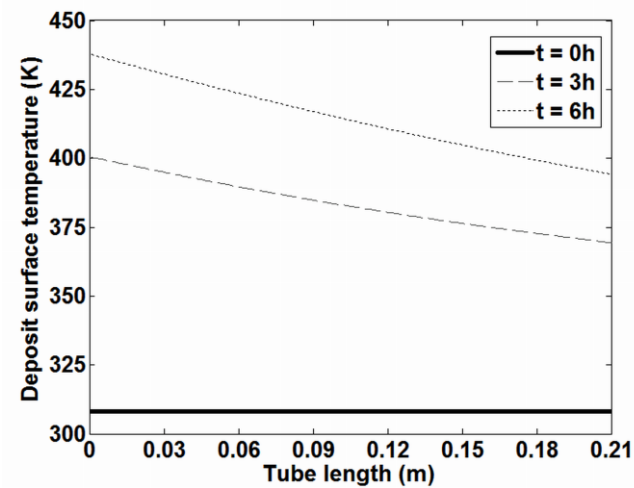
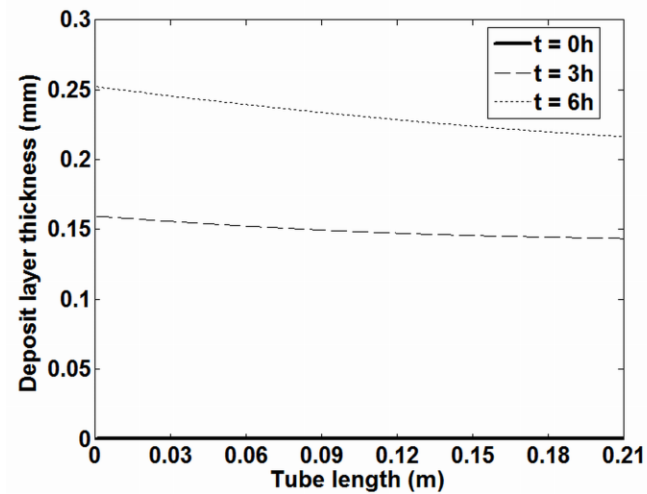
1D FOULING MODEL



Coolant Temperature: 50 °C



1D FOULING MODEL



EGR COOLER FOULING SUMMARY

- Thermophoresis is the dominant mechanism for particle deposition in EGR coolers.
- Particulate fouling can be avoided if the gas velocity through the EGR cooler is above a critical flow velocity.
- Hydrocarbon condensation has the strongest influence on deposit morphology changing it from a dry porous layer to sludge or lacquer like deposit.
- Significant removal of accumulated deposit mass was observed by using an oxidation catalyst in combination with exposure to water vapor condensation.
- Based on the findings in this study on-board “cleaning” or regeneration of the EGR cooler by exposure to water vapor condensation does seem feasible.

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OTHER PROJECTS

- Fuel Effects on Low Temperature Premixed Compression Ignition (PCI) Combustion in a Light-Duty Diesel Engine
- Characterization of Particulate Matter (PM) Emissions from a 2007 Emissions Level Heavy-Duty Diesel Engine
- Development of an Electronic Sensor for Engine Exhaust Particulate Measurements – *Doctoral Dissertation*
- Effects of In-Cylinder Wall Wetting on Size and Mass of Particulate Matter Emissions in Direct Injection Spark Ignition Engines– *Masters Thesis*
- Guest Graduate – Argonne National Laboratory
 - Used laser scattering to measure the time resolved size distribution and mass of particulate matter (PM) emissions from a direct-injection gasoline engine

Thank You